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GB 2259430 A GB 2237706 A EP 0683571 A2  
EP 0575746 A1 WO 96/08088 A1 WO 91/20142 A1  
US 5541963 A US 4278978 A

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(54) Abstract Title  
Digital radio communication system

(57) A digital radio communication system has a mobile transmitter (2) which transmits error protected digital data on a plurality of radio carriers to a plurality of receiving antennas (4). The receiving antennas are placed around an area in which the transmitter is to be used. A summation means is coupled to the receiving antennas and the signals received by them are combined to produce an output signal. The signal pulse from each receiving antenna to the summation means include delays (12, 14) to reduce the effect of interference between signals received on two or more receiving antennas. A multi-carrier receiver (10) is coupled to the summation means to receive the output signal and it includes an error protection decoder to decode the original digital data.

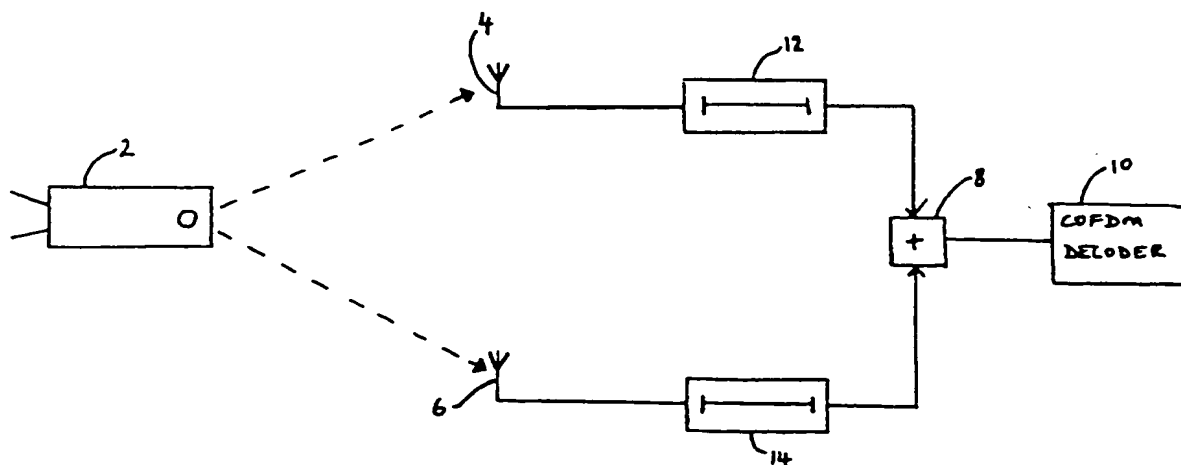


FIG. 5

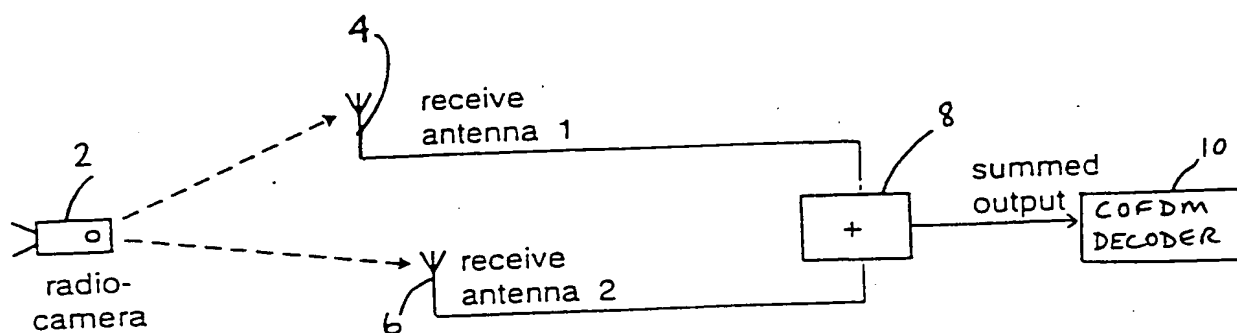


Fig. 1. Receiving the signal at two sites and summing the two signals

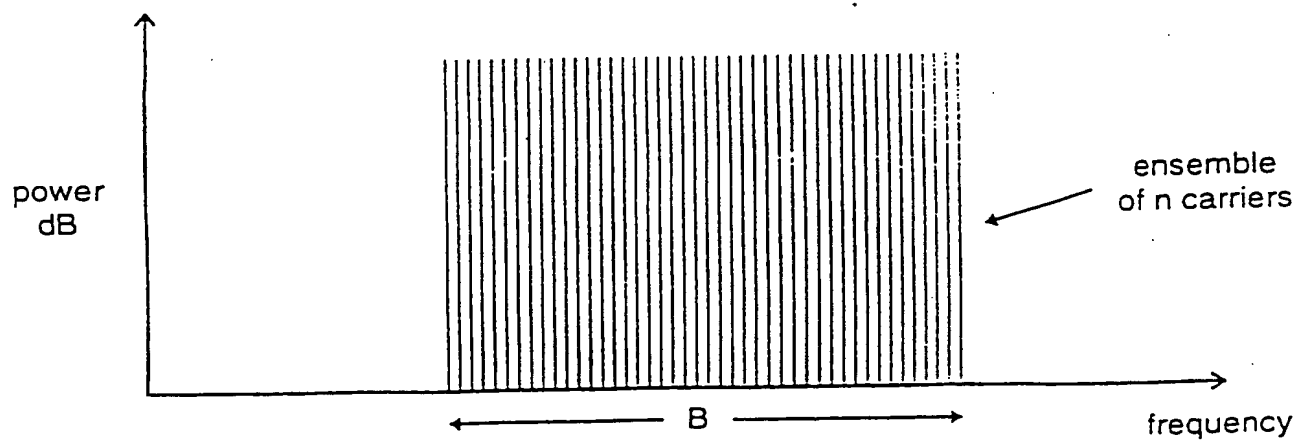


Fig. 2. Original COFDM signal generated at mobile camera.

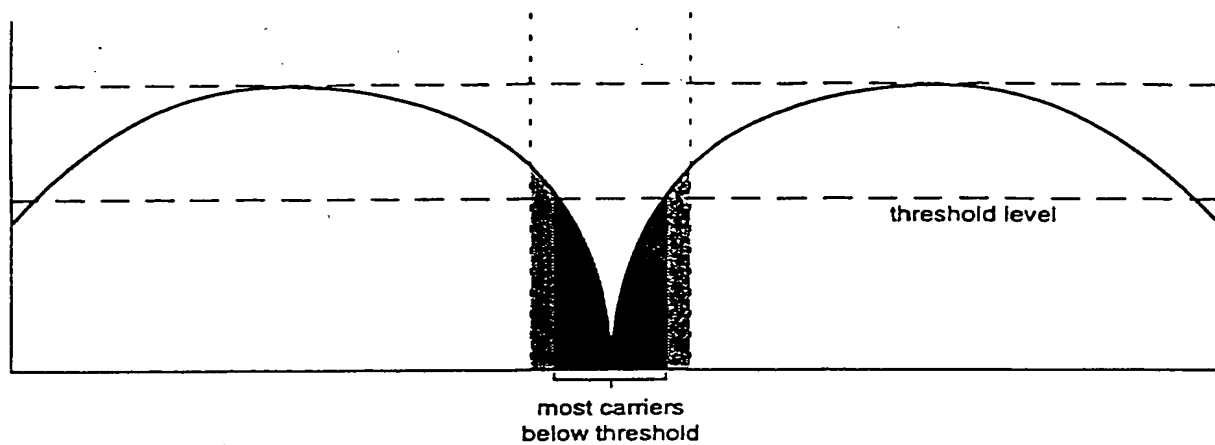
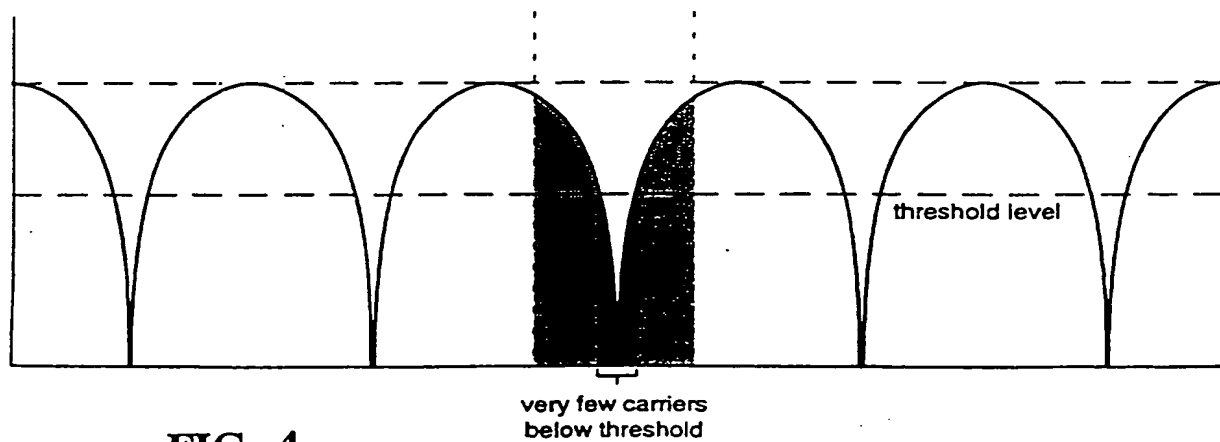
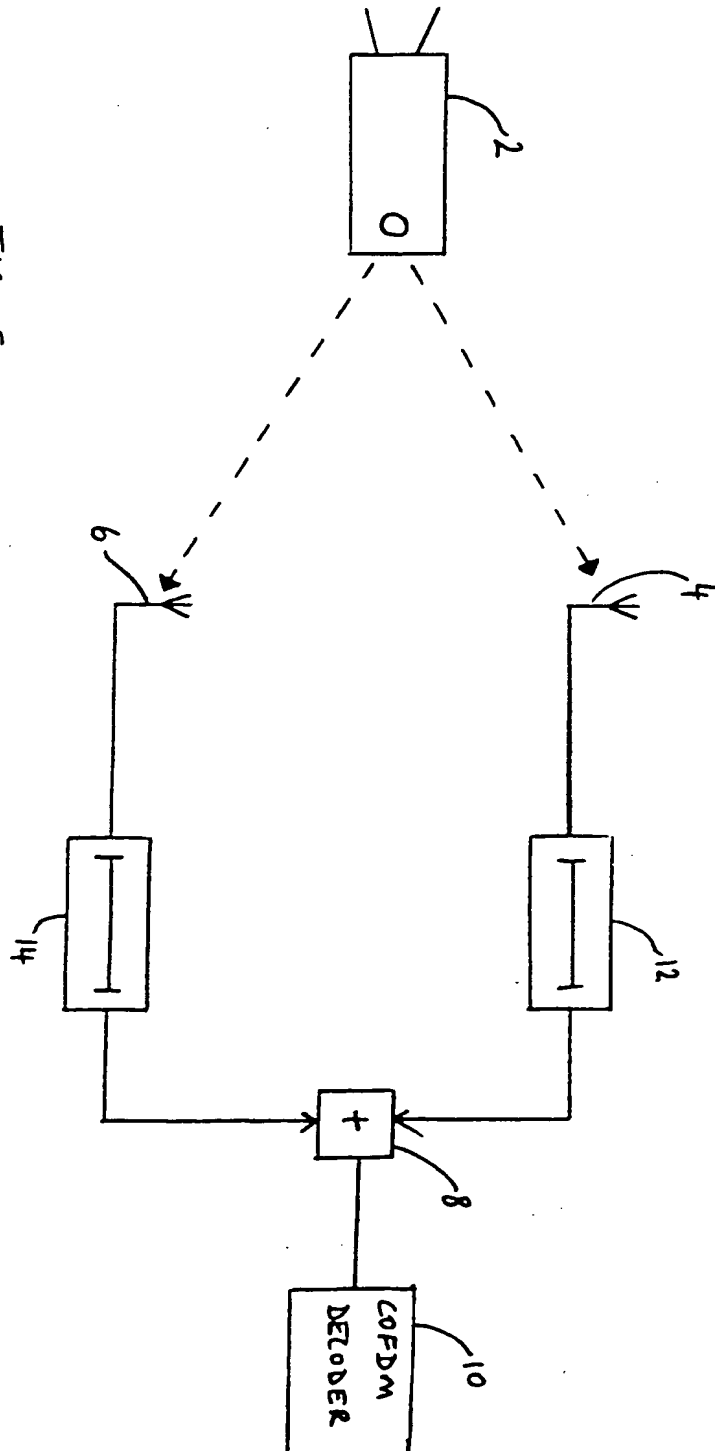
*Short delay multipath***FIG. 3***Long delay multipath (using additional delay)***FIG. 4**

FIG. 5



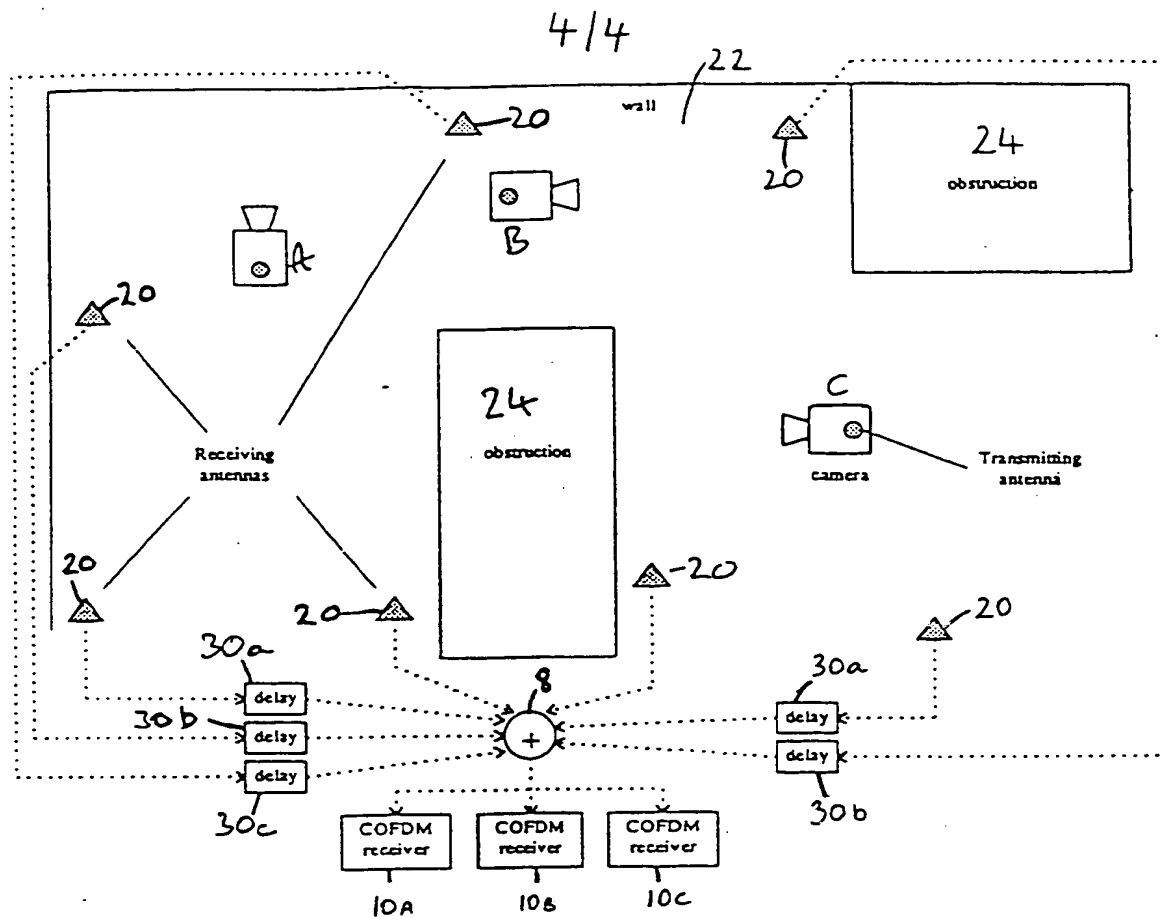


Fig. 6. An example DRUMS system

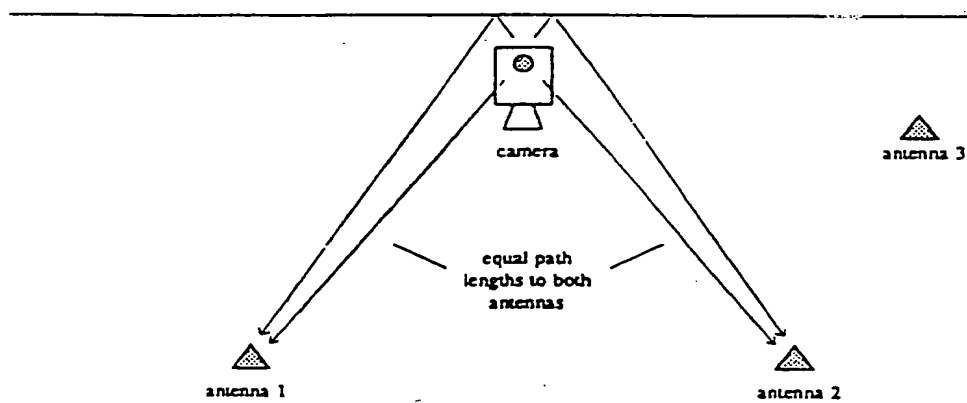


Fig. 7. Coincident flat fading at two antenna sites

DIGITAL RADIO COMMUNICATION SYSTEM

This invention relates to a digital radio communication system and, in particular, to such a system for use with a digital radio camera.

5       Analogue radio cameras are well known. These are of several types. One example is a diversity reception system in which a single transmit antenna is provided on a camera and a plurality of receiving antennas are provided around the area in which the camera operates. Each receiving  
10       antenna repeatedly monitors the strength and quality of the signal received from the radio camera and, in dependence on this information, selects which receiving antenna to use for subsequent reception of signals from the camera.

      Another type of system was proposed in our British  
15       Patent No. GB-B-2196211. In this, a plurality of directional antennas are provided on the radio camera and a single receive antenna is provided. During the field blanking intervals of a video signal a known signal is transmitted by each of the camera antennas in turn. At the  
20       receiver antenna, circuitry is provided to determine which transmit antenna gave the best signal in terms of strength and quality and a selection signal is sent back over a VHF link to the radio camera which then selects the appropriate antenna for transmission of the next field of video data.

25       The purpose of developing a digital radio camera is to provide a reliable system that is compatible with digital television production. However, simply replacing analogue modulation with digital does not necessarily provide the required degree of reliability. It is  
30       preferable for a system to be used with a simple omnidirectional antenna on a camera combined with a number of receiving antennas placed around the area of interest.

Conventional digital diversity systems rely on complex receivers at each antenna to process the signal to help decide which antenna has the best reception. These systems tend to be prohibitably expensive.

5 Preferred embodiments of the present invention seek to provide a system for use with simple receivers in order to minimise cost and to simplify operational use. In particular, a preferred embodiment provides a diversity reception system using multi-antenna summation to provide a  
10 signal.

The invention is defined in its various aspects in the appended claims to which reference should now be made.

A preferred embodiment of the invention will now be described in detail by way of example with reference to the  
15 accompanying drawings in which:

Figure 1 is a block diagram of a radio camera in a diversity reception system with signal summation;

Figure 2 is a graph of the COFDM signal generated at the mobile camera of Figure 1;

20 Figure 3 is a graph showing the summed output of the adder in Figure 1 for a small delay between the signals received at the two antennas;

Figure 4 is equivalent to Figure 3 but is a result of including a longer delay between the signals on the two  
25 antennas;

Figure 5 is a block diagram of an embodiment of the invention;

Figure 6 is a block diagram of a second embodiment of the invention; and

30 Figure 7 shows a system where a third antenna is required to avoid flat fading of the signal.

A system called Coded Orthogonal Frequency Division Multiplexing (COFDM) has been developed for Digital Audio

Broadcasting (DAB) and Digital Terrestrial Television. The bits of each digital sample are distributed over a number of spaced carriers at a number of different time intervals. The Fast Fourier Transform (FFT) of the carriers at each  
5 time interval is taken. Each FFT comprises what is known as a symbol and a plurality of these are combined into a COFDM frame. The frames are then transmitted.

The distributing of bits of data in frequency and in time gives a system which is very error resistant and can  
10 cope with a high degree of multipath distortion.

Such a system is usually used as a single frequency network with a plurality of transmitters sending out synchronised frames of data. Any multipath propagation delays in such a system will tend to be long and, as a  
15 result, any fading notches in the received signal will usually be narrow in relation to the bandwidth occupied by the complete set of carriers. Thus, only some of the carriers fade out and error correction coding can easily recover the wanted information.

20 We have appreciated that the single frequency approach can be used in reverse with a digital radio camera. All that would be needed would be to combine all the receiving antenna outputs to provide a signal to a single COFDM demodulator. This would thereby obtain the  
25 goal of having a plurality of low cost receiving sites with one complex decoder.

In the broadcasting application, the multipath propagation delays will tend to be long. As a result, any fading notches caused by multipath propagation delays will  
30 usually be narrow in relation to bandwidth of the COFDM carriers. Thus, only some of the carriers will fade out and error correction coding will be able to recover the information required.



The radio camera is likely to be used in situations, e.g., a football stadium, where the differential delays of the signal picked up at each receiving site are very small. This will cause the width of any fading notches to be  
5 large, and in some circumstances, all the carriers may be lost. For example, if the radio camera moved into a position almost exactly between two receiving antennas with cable feeds of equal length to the receiver decoder, almost all the carriers would be lost and no signal would be fed  
10 to the receiver decoder.

The type of fading which can occur is illustrated with reference to Figures 1, 2, 3 and 4. Figure 1 shows a radio camera 2 providing a COFDM signal to a pair of receive antennas 4 and 6. These in turn provide the  
15 received signals to an adder 8 which sends a summed output to a COFDM decoder.

The original COFDM ensemble of carriers generated at the radio camera is shown in Figure 2. As can be seen, all the carriers are of equal magnitude. Data is modulated  
20 onto these using a suitable modulation scheme, for example, quadrature phase shift-keying. It is of course the FFT of all these carriers which is transmitted by the camera.

Figure 3 shows the power distribution of the carriers after a reverse FFT at the COFDM decoder 10. This  
25 representation is for a small delay between the two COFDM signals. As can be seen, a large notch in the centre of the ensemble of carriers has been generated thereby losing much of the data.

In Figure 4, the same output is shown but for two  
30 signals with a much larger delay between them. The notch generated by multipath propagation is considerably narrower than in Figure 3 and thus there is sufficient data to use conventional error correction techniques to regenerate data lost in the notch.

Although the interference notch has been drawn in the centre of the COFDM ensemble in Figures 3 and 4, it can in fact occur at any point. It should be noted that as the attenuation profile is periodic, when the ensemble has a  
5 broader bandwidth, more than one notch may occur. Furthermore, the frequency spacing between the notches reduces as the delay increases thereby bringing more notches into the ensemble. The strength of COFDM is its ability to handle many notches whilst still being able to  
10 recover the signal through the use of channel coding.

It will be appreciated that there is a maximum notch width  $\Delta f$  that can be tolerated before too many carriers are lost.

The solution to the problem of wide notches being  
15 generated by digital radio cameras used in restricted environments is to add a static delay into each receiving antenna output. The value of the delay needs to be different for each antenna and large enough to ensure that the maximum notch width will never exceed a specified  
20 fraction of the bandwidth of the COFDM ensemble. The exact fraction will depend on the error correction technique, the number of antennas, and the statistical distribution of the notches. Figure 5 shows a radio camera system having a single camera and two receivers with delays included in  
25 accordance with an embodiment of the invention. As can be seen, delays 12 and 14 have been introduced in the feeds from antennas 4 and 6 to the adder 8 respectively. In practice, in a situation such as this only one delay needs to be introduced in one of the antenna feeds. However,  
30 providing delay in each feed gives a more versatile system where delays can be appropriately adjusted according to the environment in which the system is to be used.

At a complex location requiring many antennas, it is not necessary to give each antenna a unique delay. This is because the delays only need to be different for each area covered. Delay values can be re-used in different areas, providing the radio camera cannot transmit to two different antennas having the same delay as it moves from one area to the next. This avoids the problem of ending up with excessively large delays where a large number of antennas are used.

Such a system is illustrated in Figure 6. In this, a plurality of antennas 20 are provided in an area 22 bounded by a wall and having two obstructions 24. Three radio cameras are shown operating in this area and they are labelled A, B and C.

The receiving antennas 20 are all coupled to an adder 8 which provides output signals for three COFDM receivers 10, one for each radio camera.

Antennas which can not be seen by the same radio camera may have the same delay. Therefore, the two antennas 20 immediately adjacent obstruction 24 feed directly into the adder 8 with no delay. The other delays 30a, b and c are all different. However, it can be seen that two of the antennas 20 feed through a delay 30a. These again cannot be seen by one radio camera. Secondly, delays 30b cannot be seen by one radio camera. There is a final delay 30c connecting the final antenna 20 to the adder 8. The greatest delays would tend to be used in the most distant antennas to maximise effect.

An example of the technique will now be illustrated. In this example, it is assumed that a COFDM ensemble of 1,000 orthogonal carriers occupies a bandwidth of 20 MHz. This bandwidth is typical for current outside broadcast channels and will support nearly 100 Mbits per second using 64 QAM modulation (Quadrature Amplitude Modulation, a

higher level of QPSK). If the error protection provided in the COFDM gives 100 percent redundancy in the signal, then the video bit rate could be nearly 50 Mbits per second. This could be sufficient to transmit very high quality  
5 MPEG2 coded signals, provided that the guard interval between COFDM symbols is not too large. It is assumed that if a carrier in the ensemble has a level 6 dB below the largest carrier, then it is not recoverable and requires error correction to recover the data.

10 The delay lengths required are calculated by first considering the combined power,  $P(f)$ , of two interfering carriers with the same frequency that have traversed different paths:

$$P(f) = 1 + \cos\left(\frac{2\pi f l}{c}\right)$$

15 where:  $c$  is velocity of light  
 $f$  is frequency  
 $l$  is path length  
difference in vacuum

From this, it can be seen that the width of a fading  
20 notch,  $\Delta f$ , in a COFDM ensemble where carriers are weaker than -6 dB with respect to maximum power is:

$$\Delta f = \frac{100}{l} \text{ MHz}$$

If half-rate coding is used, then half the carriers can be in the notch (refers to proximation). If the COFDM

ensemble is 20 MHz wide then  $\Delta f$  will be 10 MHz which, from the above equation, gives  $l = 10$  m.

A 10 m delay is equivalent to a time period of 33 ns which is only a small fraction of a symbol period of 50  $\mu$ s  
5 In practice, an extra delay equivalent to the physical separation between the antennas is required to ensure that the signals from the radio camera can still sum with the minimum permitted differential delay in any camera position. If an area, of say, 50 m by 50 m is covered by  
10 four antennas positioned around the edges, e.g., one at each corner of the square, then the differential delay line length should be about 60 m to maintain the minimum permitted delay. This is a maximum delay of 180 m for the fourth antenna. These distances are lengths for  
15 transmissions in vacuum and it is of course better to use delay time.

The delay required is short compared to video field synchronisation, which would still be corrected by a frame store synchroniser, as is usual with radio cameras. In  
20 DAB, an extra delay is deliberately introduced by time interleaving the data as a countermeasure against fading. Time interleaving can also be used in the radio camera system. However, the diversity reception arrangement is intended to continuously present sufficient carriers to the  
25 receiver through the delayed summation process.

The length of the required delays are too long to be implemented as cable delays as losses would be too high at the typical receive microwave frequencies. Down conversion of the receive signal at the antenna to lower the cable  
30 loss or for use with an SAW delay line could be arranged. An alternative is to up convert the signal to the infra-red band and use an optical fibre as both the delay element and the interconnection cable to the summing point.

The number of antennas covering an area and their location depends on the amount of multipath distortion present. Enough antennas are needed to avoid the problem of them all receiving a signal corrupted by short delay  
5 multipath. Figure 7 shows an example where symmetry has caused antennas 1 and 2 to be affected by flat fading. In such a case, a third antenna is needed in order to recover the signal.

Even with three antennas, positions could be found  
10 where all suffer from flat fading. However, the probability is reduced in comparison with a system of just two antennas. The spatial distribution is dependent upon operating frequency.

The automatic gain control strategy for the signals  
15 received from each antenna would benefit from some form of threshold detector to avoid antennas not receiving any signal contributing noise at the summing point.

In order to undo flat fading, two or more antennas need to be summed. Each subsequent antenna must have a  
20 delay that is an integer multiple of the first delay, to avoid the delays cancelling between any pair of antennas. Thus, the first antenna has no delay, the second antenna first minimum delay, the third twice the minimum delay, and the fourth three times the minimum delay. Thus, a fourth  
25 antenna system needs a maximum delay of  $3 \times 200$ , which is 600 ns. This is just over 1 percent of the symbol rate in this example and has little effect on the channel capacity.

Making the guard interval nearly 20 times longer, e.g., 10  $\mu$ s between symbols would give a total symbol  
30 period of 60  $\mu$ s. This would still allow channel capacity of 100 Mbits per second whilst increasing the allowable antenna separation to nearly 1 km. This would be useful for e.g., helicopter operation. There are various options for implementing the delays, e.g., down conversion, SAW

delays, optical fibre delays, etc. It may be possible to  
down convert each antenna signal to produce very slightly  
different intermediate frequencies, thereby giving a  
continuously varying phase shift between them and sweeping  
5 any nulls across the pass band in the summed signal. This,  
combined with some limited time interleaving, may be of  
benefit.

At present, COFDM is limited to a gross bit rate of  
about 50 Mbits per second thereby suggesting a video bit  
10 rate of the order of 25 Mbits per second. However, the  
system does not have to be a full COFDM implementation.  
Other multicarrier or broad band techniques could be used.  
However, the application of VLSI techniques to COFDM may  
produce the compact circuitry required, possibly making it  
15 effective to obtain the required capacity by using two or  
more COFDM ensembles together.

CLAIMS:

1. A digital radio communication system comprising a mobile transmitter and a plurality of receivers for receiving signals from the transmitter, and a summation means in which signals received by the receivers are combined to provide an output signal, and wherein the signal paths from each receiver to the summation means are delayed by different amounts to reduce the effect of interference between signals received on two or more receivers.
2. A digital radio communication system according to claim 1 in which there are two or more receivers and all except one of the signal paths to the summation means includes a delay means such that signals from the receivers reach the summation means at different times.
3. A digital radio communication system according to claim 1 or claim 2 comprising at least three receivers.
4. A digital radio communication system according to any preceding claim wherein at least two of the receivers cannot simultaneously receive signals from the transmitters and the signal paths from these receivers to the summation means are delayed by similar amounts.
5. A digital radio communication system according to any preceding claim in which the transmitter transmits a COFDM signal.
6. A digital radio communication system according to any preceding claim in which there are a plurality of



transmitters provided, each transmitting signals in different parts of the frequency band.

7. A method of operating a digital radio communication system comprising a mobile transmitter and a plurality of receivers, the method comprising the step of  
5 transmitting digital signals from the transmitter, receiving the signals from the receivers, providing received signals to a summation means, and delaying the signals between the receivers and the summation means such  
10 that the effects of interference between signals are reduced.

8. A digital radio signal receiving system comprising a plurality of receivers each providing signals to a summation means, and delay means provided in at least  
15 all except one of the signal paths such that signals provided to the summation means may be delayed by different amounts to reduce the effects of interference between signals from two or more receivers.

9. A digital radio signal receiving system  
20 according to claim 8 in which the signals are COFDM signals.

10. A digital radio communication system substantially as herein described with reference to the accompanying drawings.

**Amendments to the claims have been filed as follows**

1. A digital radio communication system comprising  
a mobile transmitter for transmitting error protected  
digital data on a plurality of radio carriers to a  
5 plurality of receiving antennas for receiving signals from  
the transmitter, the receiving antenna being placed around  
an area in which the transmitter is to be used, and a  
summation means in which signals received by the receiving  
antennas are combined to provide an output signal, and  
10 wherein the signal paths from each receiving antenna to the  
summation means include delays to reduce the effect of  
interference between signals received on two or more  
receiving antennas, and a multicarrier receiver coupled to  
the summation means to receive the output signal and  
15 including an error protection decoder to decode the  
original digital data.

2. A digital radio communication system according  
to claim 1 in which there are two or more receiving  
antennas and all except one of the signal paths to the  
20 summation means includes a delay means such that signals  
from the receiving antennas reach the summation means at  
different times.

3. A digital radio communication system according  
to claim 1 or claim 2 comprising at least three receiving  
25 antennas.

4. A digital radio communication system according  
to any preceding claim wherein at least two of the  
receiving antennas cannot simultaneously receive signals  
from the transmitters and the signal paths from these  
30 receiving antennas to the summation means are delayed by  
similar amounts.

5. A digital radio communication system according to any preceding claim in which the transmitter transmits a COFDM signal.

6. A digital radio communication system according to any preceding claim in which there are a plurality of transmitters provided, each transmitting signals in different parts of the frequency band.

7. A digital radio communication system according to claim 1 in which the delay added to the signal received at each antenna has a minimum value equivalent to the maximum possible path difference between any two of the receiving antennas plus an extra delay.

8. A digital radio communication system according to claim 5 in which the maximum delay value used with one of the antennas is less than or equal to the guard interval of the COFDM signal being used.

9. A digital radio communication system according to claim 7 in which no extra delay is used with one of the antennas.

10. A digital radio communication system according to any preceding claim in which a connection means between the receiving antennas and the summation point also performs the delay function.

11. A digital radio communication system according to any preceding claim in which the received signal at each receiving antenna is converted to a different radio frequency or to an intermediate frequency or to an optical frequency to implement the delay using the appropriate connection means so that the connection means is more compact or the signal attenuation is lower.

12. A method of operating a digital radio communication system comprising a mobile transmitter for transmitting error protected digital data on a plurality of radio carriers and a plurality of receiving antennas, the  
5 method comprising the step of transmitting digital signals from the transmitter, receiving the signals from the receiving antennas, providing received signals to a summation means, delaying the signals between the receiving  
10 antennas and the summation means such that the effects of interference between signals are reduced, providing an output signal from the summation means, receiving the output signal at a receiver and decoding the output signal to decode the original digital data.

13. A digital radio communication system  
15 substantially as herein described with reference to the accompanying drawings.



Application No: GB 9725890.9  
Claims searched: 1-7

Examiner: Brian Ede  
Date of search: 22 April 1998

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:  
UK Cl (Ed.P): H4L(LDDRCP, LDDRCW, LDDRCX, LDDRQ, LDDRX, LDDSX)  
Int Cl (Ed.6): H04B 7/04 7/08 H04L 1/02 1/04 1/06  
Other: Online: WPI

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
X	GB 2259430 A (MOTOROLA) see Fig 1	1, 2, and 7
X	GB 2237706 A (RACAL) see Fig 3	1, 2, and 7
X	EP 0683571 A2 (SANYO) see 309-312 Fig 3	1, 3 and 7
X	EP 0575746 A1 (ALCATEL) see 10, 11 Fig 1	1, 2, and 7
X	WO96/08088A1 (MOTOROLA) see Fig 1	1, 2, and 7
X	WO91/20142A1 (MOTOROLA) see Fig 6	1, 3 and 7
X	US 5541963 (HITACHI) see Figs 3-5	1 and 7
X	US 4278978 (R A FROSCH) see Fig 1	1, 3 and 7

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.

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